

**Udai Pratap (Autonomous) College, Varanasi****E-learning Material**

<b>Module/ Lecture</b>	<b>11</b>
<b>Topic</b>	<b>Fourier Equation of Heat flow</b>
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## Rectilinear flow of heat along a bar : Fourier Equation of heat flow

Consider a long metal bar of uniform area of cross section 'A' heated at one end and heat flows along the length of bar. Suppose that the bar lies along x-axis whose origin lies at the hot end as shown in fig.1.

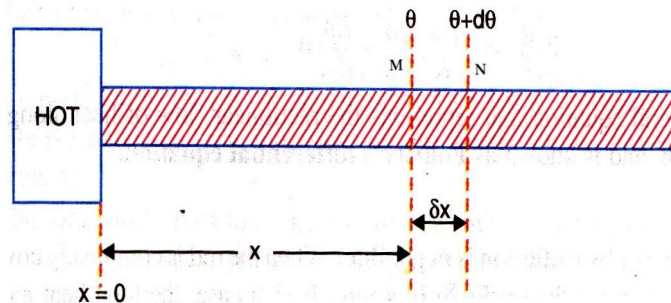


Fig. 1.

Let at a distance  $x$  from the hot end let  $\theta$  be the temperature above the surrounding and  $\frac{d\theta}{dx}$  be the temperature gradient, at any time. Consider two planes M and N perpendicular to the length of the bar at distance  $x$  and  $x + \delta x$  from the hot end i.e. thickness of section MN will be  $\delta x$ . Also the temperature at N will be  $\theta + \frac{\partial \theta}{\partial x} \delta x$  and the temperature gradient at N will be  $\frac{d}{dx} \left( \theta + \frac{\partial \theta}{\partial x} \delta x \right)$ .

The heat flowing per second into the element at M is

$$Q_1 = -KA \frac{d\theta}{dx} \quad (1)$$

Where K is the coefficient of thermal conductivity.

Also, the heat flowing out per second from the element at N is

$$Q_2 = -KA \frac{d}{dx} \left( \theta + \frac{\partial \theta}{\partial x} \delta x \right)$$

$$= -KA \frac{d\theta}{dx} - KA \frac{\partial^2 \theta}{\partial x^2} \delta x \quad (2)$$

Thus the heat gained by the section MN per second

$$Q = Q_1 - Q_2 = KA \frac{\partial^2 \theta}{\partial x^2} \delta x \quad (3)$$

Before the steady state is reached, the quantity of Q is used (i) partially to raise the temperature of the bar say,  $Q_i$  and (ii) partially radiated out, say  $Q_r$ , i.e.

$$Q = Q_i + Q_r \quad (4)$$

Let  $\frac{\partial \theta}{\partial t}$  be the rate of rise of temperature of rod at section MN. The heat used per second to raise the temperature of the bar at section MN will be

$Q_i = \text{mass} \times \text{specific heat} \times \text{rate of increase of temperature}$

$$Q_i = (A\delta x) \rho s \frac{\partial \theta}{\partial t}$$

$$Q_i = (A\delta x) \rho s \frac{\partial \theta}{\partial t} \quad (5)$$

where 'A' is the area of cross section of bar,  $\rho$  is the density of material of bar, s is the specific heat of the material of bar.

The heat lost due to radiation will be

$$Q_r = E p \delta x \theta \quad (6)$$

Where E is the emissive power of the surface of bar, p is the perimeter of the surface,  $\theta$  be the average excess temperature above the surrounding of the bar between M & N.

Thus from Equations (3, 4, 5 & 6) we get,

$$KA \frac{\partial^2 \theta}{\partial x^2} \delta x = (A\delta x) \rho s \frac{\partial \theta}{\partial t} + E p \delta x \theta$$

$$\text{i.e.} \quad \frac{\partial^2 \theta}{\partial x^2} = \frac{\rho s}{K} \frac{\partial \theta}{\partial t} + \frac{E_p}{KA} \theta \quad (7)$$

This is the general equation for rectilinear flow of heat along a bar and it is known as Fourier Equation of Heat flow.

Now we will consider some particular cases of interest

- 1. Steady State:** In this state, which is attained after some time, temperature of section MN does not change with time, i.e.

$$\frac{\partial \theta}{\partial t} = 0$$

Thus Equation (7) reduces to

$$\frac{\partial^2 \theta}{\partial x^2} - \frac{E_p}{KA} \theta = 0 \quad (8)$$

We see that  $\theta$  is the function of  $x$  only and we consider following two cases:

- (i). Radiation from the surface of the bar is allowed:** If the bar is not insulated the Eq.(8) is

$$\frac{\partial^2 \theta}{\partial x^2} - \frac{E_p}{KA} \theta = 0$$

$$\frac{\partial^2 \theta}{\partial x^2} - \alpha^2 \theta = 0 \quad (9)$$

**Where**  $\alpha^2 = \frac{E_p}{KA}$

General solution of the equation (9) is

$$\theta = b_1 e^{\alpha x} + b_2 e^{-\alpha x} \quad (10)$$

Where  $b_1$  and  $b_2$  are constants which can be determined by knowing the boundary conditions. Let the boundary conditions

For  $x=0$ ,  $\theta = \theta_0$  and for  $x=\infty$ ,  $\theta = 0$  (i.e. the cold end is at the temperature of surrounding). Using these boundary conditions we get  $b_1=0$  and  $b_2 = \theta_0$  and from Eq. (10) we get

$$\theta = \theta_0 e^{-\alpha x} \quad (11)$$

Eq. (11) gives the excess of temperature above the surrounding at any point at distance  $x$  along the bar, exposed to the radiation, after steady state is reached. We see that  $\theta$  is an exponential function of distance  $x$  of the point from the hot end and is independent of time.

**(ii). Radiation from the surface of the bar is not allowed:** If the bar is insulated, there will be no loss of heat from the surface of the rod, i.e.  $E=0$  in Eq. (8), and from (8) we get

$$\frac{\partial^2 \theta}{\partial x^2} = 0 \dots\dots\dots (12)$$

On solving Eq. (9) we get

$$\theta = c_1 x + c_2 \quad (13)$$

Where  $c_1$  and  $c_2$  are constants which can be determined by knowing the temperatures at the two points on the bar,

$$\text{If } x=0, \theta = \theta_0 \text{ and at } x=l, \theta = \theta_1 \text{ then } c_2 = \theta_0 \text{ and } c_1 = -\frac{\theta_0 - \theta_1}{l}$$

and therefore

$$\theta = \theta_0 - \frac{(\theta_0 - \theta_1)}{l} x \quad (14)$$

Equations (14) gives the excess temperature above surrounding at any point  $x$  along the insulated bar.

2. **Variable State:** If the heat lost by radiation is negligible ( $E=0$ ), the equation (7) reduces to

$$\frac{\partial^2 \theta}{\partial x^2} - \frac{\rho s}{K} \frac{\partial \theta}{\partial t} = 0$$

**or** 
$$\frac{\partial \theta}{\partial t} = h \frac{\partial^2 \theta}{\partial x^2} \quad (15)$$

Quantity  $h = \frac{K}{\rho s}$  is called diffusivity which determines the rate at

which temperature change takes place in the bar. The above equation can be solved when variation of  $\theta$  with time is known.